

# Morphology Optimization of Silver Nanoparticles Used to Improve the Light Absorption in Thin-Film Silicon Solar Cells

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**Abstract** Silver nanoparticle (NP) arrays are used as antireflection coating to enhance light trapping capability of thin-film silicon solar cells. In this paper, we theoretically investigate the differences of light absorption distribution between the silver NP (spherical and hemispherical) array layer and the crystalline silicon (CS) substrate. Compared to the naked silicon of the same thickness, the results show that only the flattened hemispherical silver NPs can really improve the light trapping ability and make the light absorption of CS body increase by 26%; the optimum ratio of lateral (NP diameter divided by the array periodicity) and longitudinal (NP height divided by diameter) are 0.86 and 0.22, respectively.

**Keywords** Antireflection coatings · Geometric optical design · Thin films · Nanomaterials

## Introduction

Metal nanoparticle (NP) arrays can interact intensively with the incident sunlight and harvest it because they have surface plasmons. The captured energy carried by sunlight is confined to metal NP surfaces and used to increase the local

temperature, generate hot electrons, and enhance localized electric field through different mechanisms [1, 2]. A lot of papers have investigated these mechanisms and applied them in NP-enhanced optoelectronic devices successfully [3, 4]. In thin-film solar cells, based on diffraction coupling of localized plasmons in which resonance occurs mostly in the visible or infrared region of the electromagnetic spectrum, metal NPs are also used as plasmonic antireflection coatings to increase the light absorption [5–7]. The optical properties of metal NPs are affected by their shape and size, the length of arrays, the dielectric constant of surrounding medium, and so on [8–11]. This article studies the optical properties of thin-film silicon solar cells from a different point of view, the difference of light absorption distribution between the antireflection coating and the crystalline silicon (CS) body.

In the experiment, the metal NP layer and thin-film substrate are considered as one whole body so as to discuss the optical properties, and the difference of light absorption distribution between them is not distinguishable. However, in theory, they can be discussed as two different parts separately. Therefore, this study is different from the previous ones in that it focuses and emphasizes on the distribution of absorbed photons in the two parts. As shown in Fig. 1a, the total light absorption ( $A$ ) can be divided into two parts:  $A = A_{Ag} + A_{Si}$ .  $A_{Ag}$  is one part which has been absorbed by silver NP array layer and  $A_{Si}$  is the other part which has been absorbed by thin-film CS substrate. So, in order to get better and effective light absorption, there is need not only to reduce the light reflection ( $R$ ) and transmission ( $T$ ) but also to decrease the proportion of  $A_{Ag}$  in the total absorption, which can be easily seen from the formula  $A_{Si} = 1 - R - T - A_{Ag}$ .

Considering each absorbed photon with energy greater than the band gap produces one and only one electron-hole pair, for the purpose of quantitative comparison, compared to the naked CS with the same thickness, two enhancement

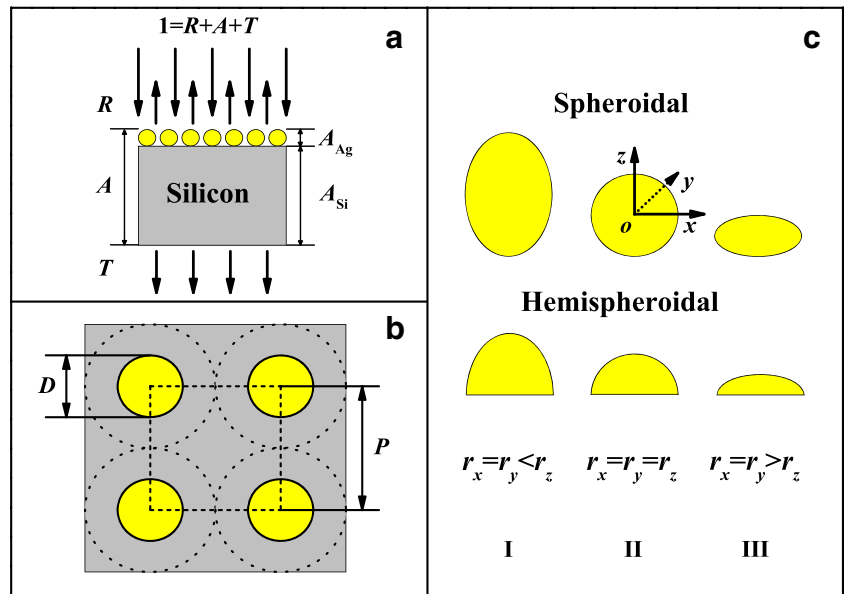
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**Fig. 1** **a** Distribution of light absorption ( $A_{Ag}$  and  $A_{Si}$  are light absorptions of silver NP antireflection layer and CS body, respectively). **b** Structure diagram of NP arrays ( $D$  is the NP diameter;  $P$  is the period length). **c** Different shapes of NPs with spheroidal and hemispheroidal (I,  $r_x = r_y < r_z$ ; II,  $r_x = r_y = r_z$ ; III,  $r_x = r_y > r_z$ )



factors of efficient light trapping  $E_T$  and effective light absorption  $E_A$  are defined as follows:

$$E_T = \frac{N_t - N_{nSi}}{N_{nSi}} \tag{1}$$

$$E_A = \frac{N_{Si} - N_{nSi}}{N_{nSi}} \tag{2}$$

here,

$$N_t = \int A(\lambda) F(\lambda) \lambda / (h_0 c_0) d\lambda \tag{3}$$

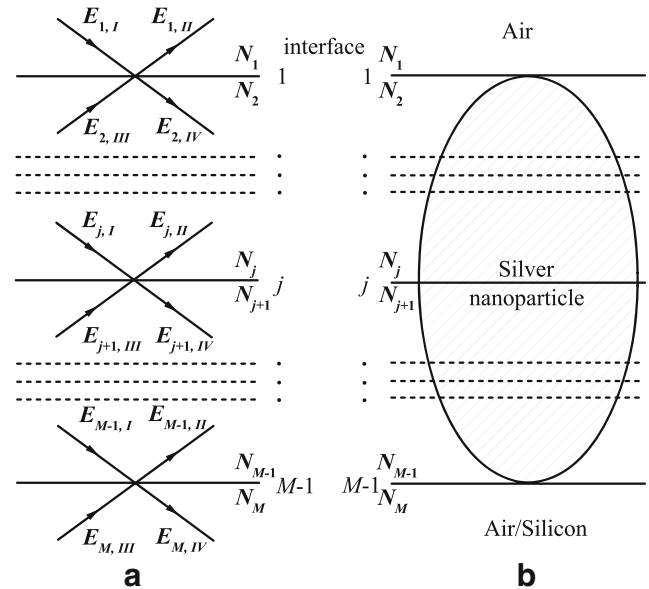
$$N_{Si} = \int A_{Si}(\lambda) F(\lambda) \lambda / (h_0 c_0) d\lambda \tag{4}$$

$$N_{nSi} = \int A_{nSi}(\lambda) F(\lambda) \lambda / (h_0 c_0) d\lambda \tag{5}$$

$N_t$  is the total number of absorbed photons in the whole body including the CS substrate and metal NP antireflective coating.  $N_{Si}$  is the number of absorbed photons in the CS substrate which is a part of the whole, and  $N_{nSi}$  is the number of absorbed photons of the naked CS.  $A(\lambda)$ ,  $A_{Si}(\lambda)$ , and  $A_{nSi}(\lambda)$  are the corresponding light absorption coefficient.  $F(\lambda)$  is the distribution of solar radiation spectral intensity on the Earth’s surface under AM 1.5 spectrum [12].  $\lambda$  is the wavelength of incident light;  $h_0$  and  $c_0$  are Planck constant and speed of light in vacuum, respectively. As shown in Fig. 1b, c, the metal NPs with the diameter of  $D$  are arranged in a square array with array length of  $P$ , and two shapes of NPs (spheroidal and hemispheroidal) with different sizes are taken into consideration.

### Simulation Methods

In our theoretical calculations, the net radiation method [NRM] is used because it provides good matching between simulation and experimental results [13–15]. Moreover, it is very suitable for calculating the reflection, transmission, and absorption characteristics of each layer in a multilayer medium system. As shown in Fig. 2a, a system of  $M$  layers,  $I$ ,  $III$  and  $II$ ,  $IV$  represent the incoming and outgoing electromagnetic radiation fluxes ( $E$ ), respectively. The interfaces are labeled  $j$



**Fig. 2** **a** Schematic multilayer structure, with numbering convention of interfaces (1, ...,  $j$ , ...,  $M - 1$ ), complex refractive index ( $N_1, \dots, N_j, \dots, N_M$ ), and electromagnetic radiation fluxes ( $E_{j,I}, E_{j,II}, E_{j+1,III}, E_{j+1,IV}, \dots$ ). **b** Schematic representation of silver NP and effective multilayer structure

( $j = 1, \dots, M - 1$ ) and the complex refractive index of  $j$ -th medium is  $N_j$ . For every interface  $j$ , there are four equations and the relations between the incoming and outgoing electromagnetic radiation fluxes can be expressed as follows:

$$\begin{cases} E_{j,I} = \tau_j E_{j,IV} \\ E_{j,II} = r_{j,j+1} E_{j,I} + t_{j+1,j} E_{j+1,III} \\ E_{j+1,III} = \tau_{j+1} E_{j+1,II} \\ E_{j+1,IV} = t_{j,j+1} E_{j,I} + r_{j+1,j} E_{j+1,III} \end{cases} \quad (6)$$

The reflection and transmission coefficient at each of the interface are  $r_{j,j+1}$  and  $t_{j,j+1}$  which are determined using Fresnel’s laws;  $\tau_j$  is the absorption attenuation rate of layer  $j$ , defined by

$$\tau_j = \exp(-\alpha d_j / \cos \varphi) \quad (7)$$

where  $\alpha = 4\pi k_j / \lambda$  is the absorption coefficient and  $d_j / \cos \varphi$  is the distance that electromagnetic radiation travels through the layer of thickness  $d_j$  with propagation angle  $\varphi$ .  $k_j$  is the imaginary part of the complex refractive index  $N_j = n_j - ik_j$ . Both the real refractive index  $n_j$  and the extinction coefficient  $k_j$  are functions of  $\lambda$ . Assuming the incident electromagnetic radiation flux  $E_{1,I} = 1$  and  $E_{M,III} = 0$ , then, for each layer  $j$ , the spectral reflectance  $R_j = E_{j-1,II}$ , transmittance  $T_j = E_{j+1,IV}$  and absorptance  $A_j = E_{j,II} - E_{j,III} + E_{j,IV} - E_{j,I}$  can be worked out.

The effective multilayer structure of metal NPs is shown in Fig. 2b, and the complex dielectric constant

of different NP layers can be solved by the effective medium approximation which is appropriate for combining both the metal particles and medium [16]:

$$\frac{\epsilon_c - \epsilon_0}{\epsilon_c + 2\epsilon_0} = f \frac{\epsilon_{Ag} - \epsilon_0}{\epsilon_{Ag} + 2\epsilon_0} \quad (8)$$

where  $f$  is the ratio of volume filling of metal NPs.  $\epsilon_0$ ,  $\epsilon_{Ag}$ , and  $\epsilon_c$  are the complex dielectric constants of air, silver [17], and the interlayer of silver NPs, respectively.

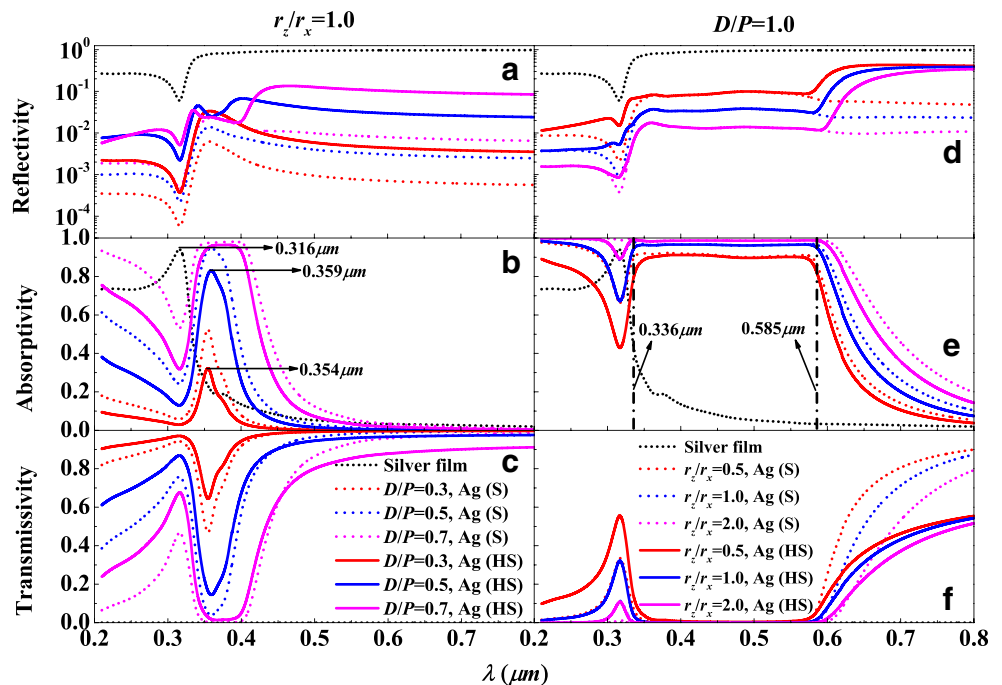
Before starting the calculations, related parameters are assumed as follows: the diameter of silver NPs can change from 0 to 200 nm which is also the maximum value of array length  $P$  and the thickness of CS substrate is 100  $\mu\text{m}$ ; the layer thickness  $d_j = 1$  nm and it is also the minimum step in calculating.

### Results and Discussion

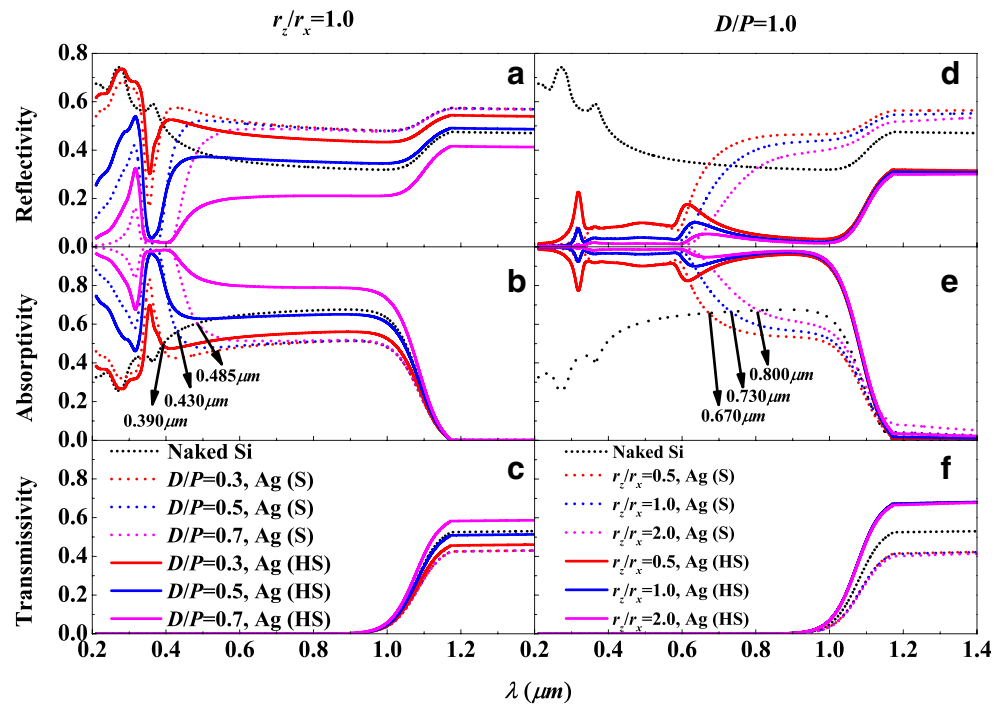
Compared to the continuous silver film, silver NPs have very different optical properties and they depend on the NP shapes and sizes. Under the different parameters, the light reflectivity, absorptivity, and transmissivity of silver NPs surrounded by air are shown in Fig. 3. Figure 4 shows the results when silver NPs are used as antireflection coating on the CS substrate.

For the continuous silver film, there is an obvious characteristic absorption peak at the wavelength of 0.316  $\mu\text{m}$ . Most of the light ( $\lambda > 0.316 \mu\text{m}$ ) is fully reflected and the transmitted light is almost zero which are shown in Fig. 3. However,

**Fig. 3** Optical properties of silver NPs (spheroidal (S) and hemispheroidal (HS)) surrounded by air under different parameters compared to the silver film with a thickness of 100 nm. **a, b,** and **c** are the light reflectivity, absorptivity, and transmissivity of different ratios of  $D/P$  (0.3, 0.5, and 0.7) under  $r_z/r_x = 1.0$ , respectively. **d, e,** and **f** are the light reflectivity, absorptivity, and transmissivity of different ratios of  $r_z/r_x$  (0.5, 1.0, and 2.0) under  $D/P = 1.0$ , respectively



**Fig. 4** Optical properties of CS with silver NPs (spheroidal (S) and hemispheroidal (HS)) as antireflection coating under different parameters compared to the naked silicon. **a, b, and c** are the light reflectivity, absorptivity, and transmissivity of different ratios of  $D/P$  (0.3, 0.5, and 0.7) under  $r_z/r_x = 1.0$ , respectively. **d, e, and f** are the light reflectivity, absorptivity, and transmissivity of different ratios of  $r_z/r_x$  (0.5, 1.0, and 2.0) under  $D/P = 1.0$ , respectively

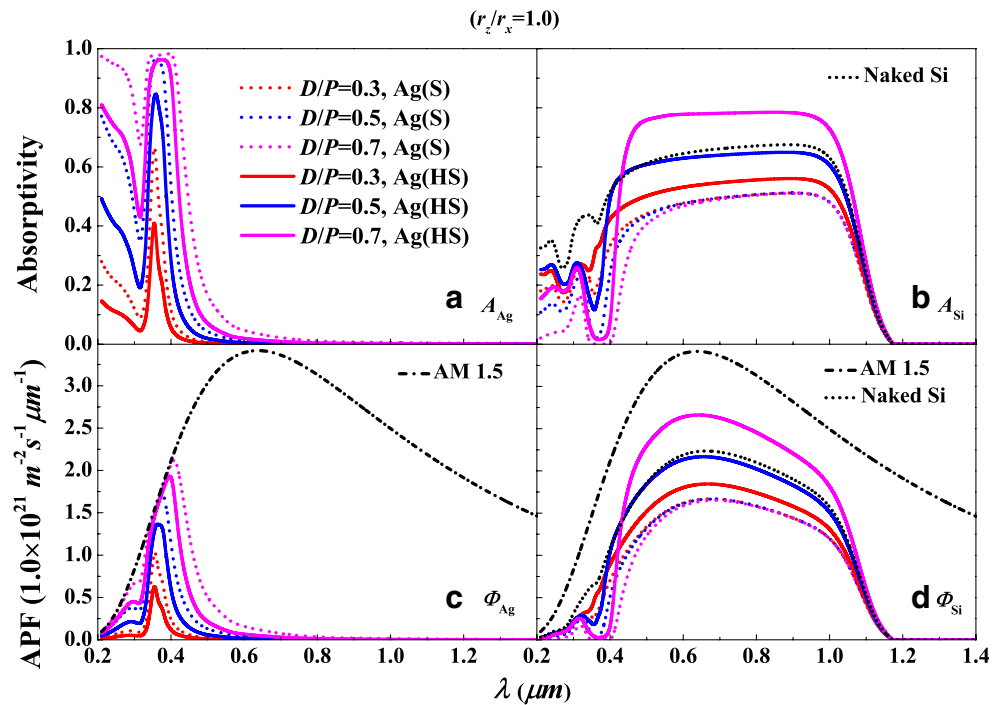


for the discontinuous silver NPs, at the same wavelength, the absorption peak which occurred in the continuous silver film is reversed and changed into transmission peak [9, 18, 19]. Under  $r_z/r_x = 1.0$ , with increase in silver NP diameter, one or two peaks appear in the light reflection of the two shapes of NPs (Fig. 3a), and they have the trend to shift to long wavelength direction. The reflection is also stronger with the larger diameter especially at long wavelengths and the hemispheroidal NPs have larger light reflection than the spheroidal NPs. For the light absorption (Fig. 3b), both shapes of silver NPs form new absorption peaks at the same position and they are only correlated with the transverse diameter (The absorption peaks are at the wavelength of  $0.354 \mu\text{m}$  for  $D/P = 0.3$  and  $0.359 \mu\text{m}$  for  $D/P = 0.5$ ). Moreover, with the increase of transverse diameter, absorption intensity also increases and absorption peaks begin to gradually widen when  $D/P \geq 0.6$ , and eventually, they become flat which means there is strong light absorption. In addition, the spheroidal NPs have larger absorption than the hemispheroidal NPs because of the larger volume. This is shown in Fig. 3b, e. Under  $D/P = 1.0$ , as shown in Fig. 3d–f, different values of  $r_z$  mainly affect the intensity of the light absorption, reflection, and transmission. When the value of  $r_z$  is bigger, there is stronger and broader absorption between  $0.336$  and  $0.585 \mu\text{m}$ , and there is only a slight difference between the two shapes. Overall, the transverse diameter of silver NPs is an important parameter that it determines the wavelength range of sunlight band absorption [20, 21], and  $r_z$  is related to the strength of the light absorption. In addition, spheroidal silver NPs have less light reflection and more transmission than hemispheroidal silver NPs especially

when the wavelength is greater than  $0.585 \mu\text{m}$  as shown in Fig. 3d, f.

Because of the better light trapping by silver NPs shown in Fig. 3, they can be used as antireflection coating to improve the light absorption of CS thin-film solar cells. As shown on the left side of Fig. 4, under  $r_z/r_x = 1.0$ , compared with Fig. 3a, b, the total light reflection is enhanced due to the presence of silicon surface; meanwhile, the total light absorption is also improved owing to the absorption of CS body. However, compared with the bare silicon shown in Fig. 4a, b, with the increase of hemispheroidal silver NP diameter, the antireflection and absorption are significantly improved when the ratio of  $D/P$  is greater than 0.5. However, for spheroidal silver NPs, in the majority absorption band of CS, there is strong light reflection effect which is bound to lead to the weakening of light absorption when the wavelength is longer than the transition wavelength (The transition wavelengths are  $0.390 \mu\text{m}$  for  $D/P = 0.3$ ,  $0.430 \mu\text{m}$  for  $D/P = 0.5$ , and  $0.485 \mu\text{m}$  for  $D/P = 0.7$ , respectively), and it can be used to explain why the silicon absorption enhancement is mainly in the shorter wavelengths mentioned in Xu et al.'s [9] study. In the same way, under  $D/P = 1.0$ , as shown on the right side of Fig. 4, the longitudinal diameter of silver NPs mainly affects the intensity of the light absorption, reflection, and transmission. For spheroidal NPs, there is also a transition wavelength for the different values of  $r_z$  (The transition wavelengths are  $0.670 \mu\text{m}$  for  $r_z/r_x = 0.5$ ,  $0.730 \mu\text{m}$  for  $r_z/r_x = 1.0$ , and  $0.800 \mu\text{m}$  for  $r_z/r_x = 2.0$ , respectively); when the wavelength is greater than the transitional wavelength, the light absorption and reflection properties become worse than bare CS. For hemispheroidal NPs, it seems

**Fig. 5** Under  $r_z/r_x = 1.0$ , **a** and **c** are the light absorptivity  $A_{Ag}$  and absorptivity of photon flux (APF)  $\Phi_{Ag}$  of silver NP coating, respectively; **b** and **d** are respectively the light absorptivity  $A_{Si}$  and APF  $\Phi_{Si}$  of CS body compared to the bare silicon under AM. 1.5 spectrum

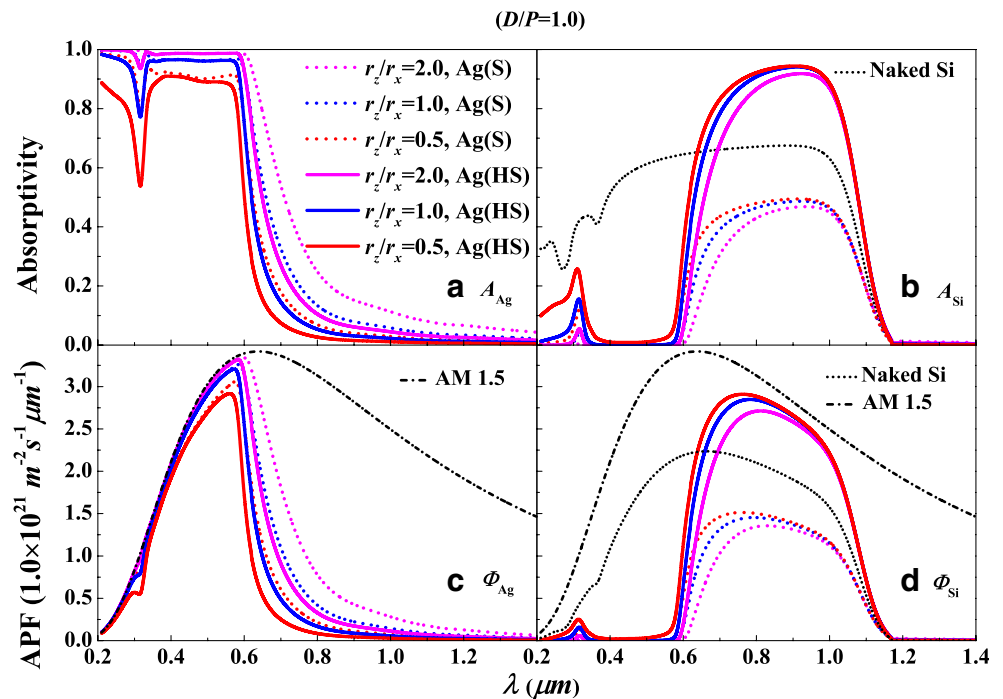


the bigger the longitudinal diameter, the better the optical properties. Moreover, the larger spheroidal NPs can enhance the absorption of infrared light as shown in Fig. 4e.

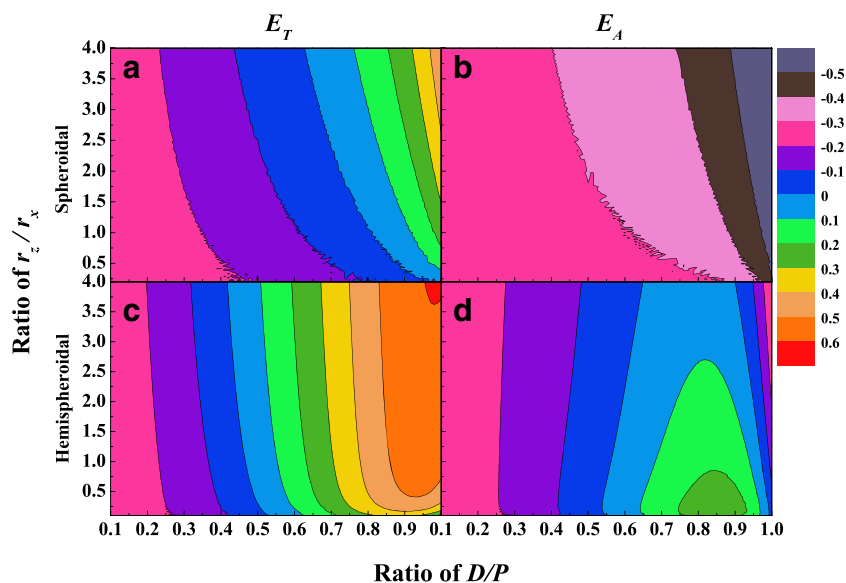
For the thin-film silicon solar cells, the two shapes of silver NPs result in completely different optical properties in the middle- and long-wave infrared regions. On the one hand, optical properties depend on the shapes and sizes of silver NPs, and on the other hand, the interface between hemispheroidal NPs and CS body is a flat surface, not a point

contact, which greatly improves the path length and increases the light absorption in the CS body. Therefore, it can be concluded that hemispheroidal silver NPs as an antireflection coating can greatly enhance light absorption in thin-film silicon solar cells, and the larger the volume, the stronger the light absorption property as depicted in Fig. 4e. However, most of the light absorbed by silver NPs is used to generate heat and is hence a waste of light for thin-film solar cells. For this reason, the difference of light absorption distribution between the

**Fig. 6** Under  $D/P = 1.0$ , **a** and **c** are the light absorptivity  $A_{Ag}$  and absorptivity of photon flux (APF)  $\Phi_{Ag}$  of silver NP coating, respectively; **b** and **d** are respectively the light absorptivity  $A_{Si}$  and APF  $\Phi_{Si}$  of CS body compared to the bare silicon under AM. 1.5 spectrum



**Fig. 7** **a**, **b**, **c**, and **d** are contour maps of enhancement factors  $E_T$  and  $E_A$  under different values of  $r_z/r_x$  and  $D/P$ , which correspond to the spheroidal and hemispheroidal silver NPs



silver NP antireflection layer and CS body should be further studied in order to obtain the appropriate parameters.

The total light absorption can be divided into two parts such that  $A=A_{Ag}+A_{Si}$  as shown in Fig. 1a. The distribution of light absorption between them is calculated and shown in Figs. 5 and 6 under different parameters. Compared to silver NPs exposed in the air (Fig. 3b, e), silver NPs on the CS thin film show a subtle increase in the light absorption because of the multiple light reflection between the contact interfaces, as shown in Figs. 5a and 6a. With silver NPs as an antireflection coating, the larger the diameter of the NPs, the more the absorption of the middle- and long-wave infrared regions as seen on the left side of Fig. 6. But with CS body, in the region where the main light absorption and conversion take place, the absorption of medium and short waves decreases due to the intense absorption by silver NPs seen from the right side of Figs. 5 and 6. More importantly, for spheroidal silver NPs, there is no improvement in photon absorption in the CS body no matter how big the diameter or volume is. However, for hemispheroidal silver NPs, it is beneficial for efficiency of photon harvesting enhancement when with proper parameters.

Increasing the amount of photons which can be absorbed by CS body compared to the bare CS is what an antireflection coating does. To make the difference more intuitionistic between the silver NP coating and CS body, the three-dimensional illustration is shown in Fig. 7. As shown, two enhancement factors, namely efficient light trapping  $E_T$  and effective light absorption  $E_A$ , are used to quantitatively contrast the optical properties of the two shapes of silver NPs. For spheroidal NPs (Fig. 7a, b),  $E_T$  can reach more than 0.4, but  $E_A$  is negative and far less than zero. For hemispheroidal silver NPs, when the ratio of  $D/P$  approaches 1.0 and the ratio of  $r_z/r_x$  is greater than 4.0,  $E_T$  can reach more than 0.6. However,  $E_A$  has maximum value of about 0.26 when the ratio of  $D/P$  nears

0.86 and  $r_z/r_x$  approaches 0.22. In conclusion, Fig. 6 shows that spheroidal silver NPs are useless and not effective in improving the photon absorption of CS body. On the contrary, the hemispheroidal silver NPs, especially the flat hemispheroidal NPs, can greatly improve the light absorption of thin-film silicon solar cells, and this is in agreement with the similar results from other studies [7, 10, 22, 23]. Moreover, it is worth noting that in the optimum range,  $E_T$  is only about 0.40, not the biggest value 0.6, which means the pursuit of the best light trapping properties should take into consideration effective light absorption.

## Conclusions

We have investigated the light trapping and the light absorption properties of two shapes (spheroidal and hemispheroidal) of silver NPs as antireflection coating for thin-film silicon solar cell. For the convenience of quantitative evaluation, two enhancement factors  $E_T$  and  $E_A$  are introduced, and the results show that spheroidal silver NPs are not suitable for use as antireflection coating due to their strong light absorption characteristics. However, the hemispheroidal silver NPs especially the flat NPs can be used for the enhancement of light transmission for silver NPs and increase light absorption for the thin-film silicon solar cells.

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